

# Design and Performance of New High Resolution MALDI-TOF Mass Spectrometers

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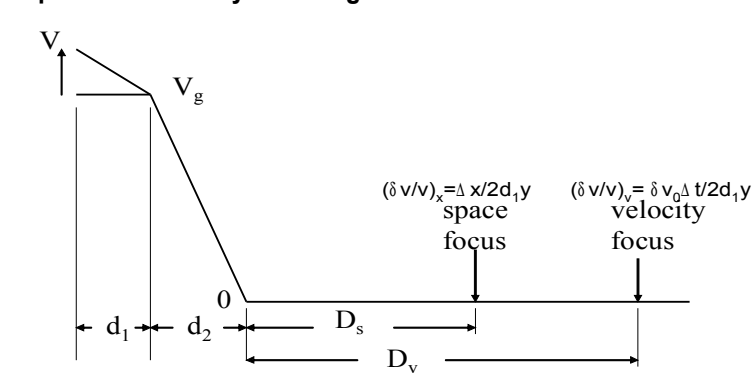
## Introduction

In earlier work, theoretical techniques for optimizing the resolving power of MALDI TOF MS systems were presented, and validated for a single reflector instrument. In the work presented here, all of the known contributions to peak width are considered and ultimate limits with presently available technology are defined.

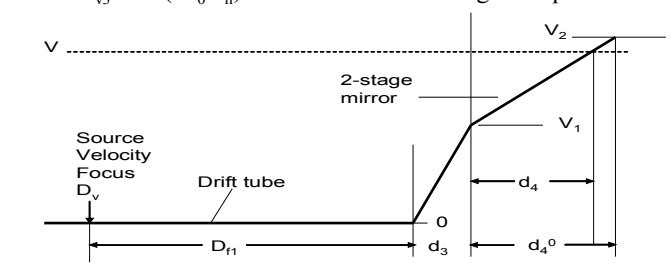
## Objective

Establish the practical limits on performance of MALDI-TOF instruments and design and build instruments that test these limits.

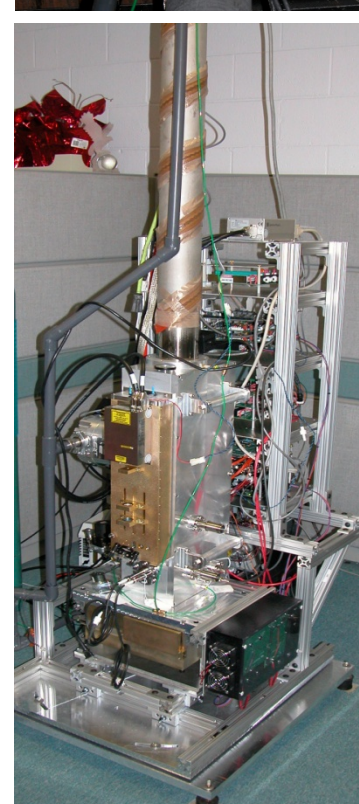
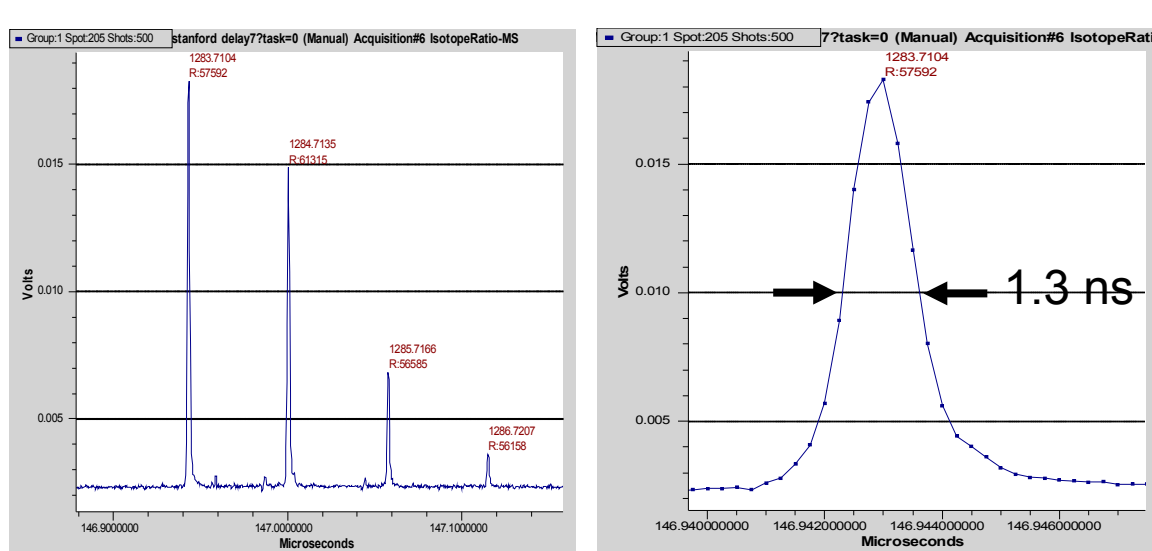
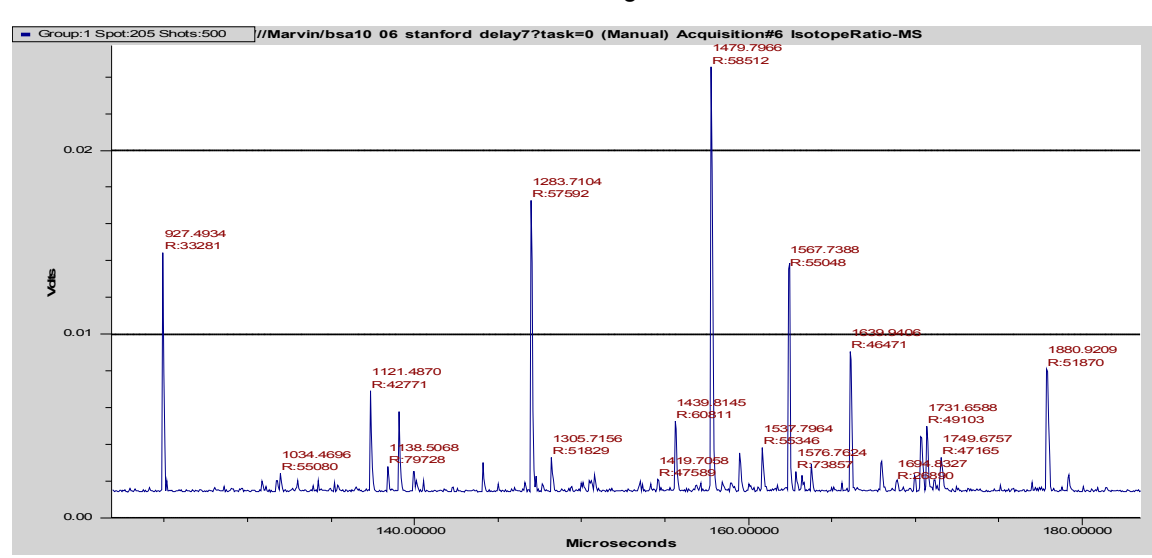
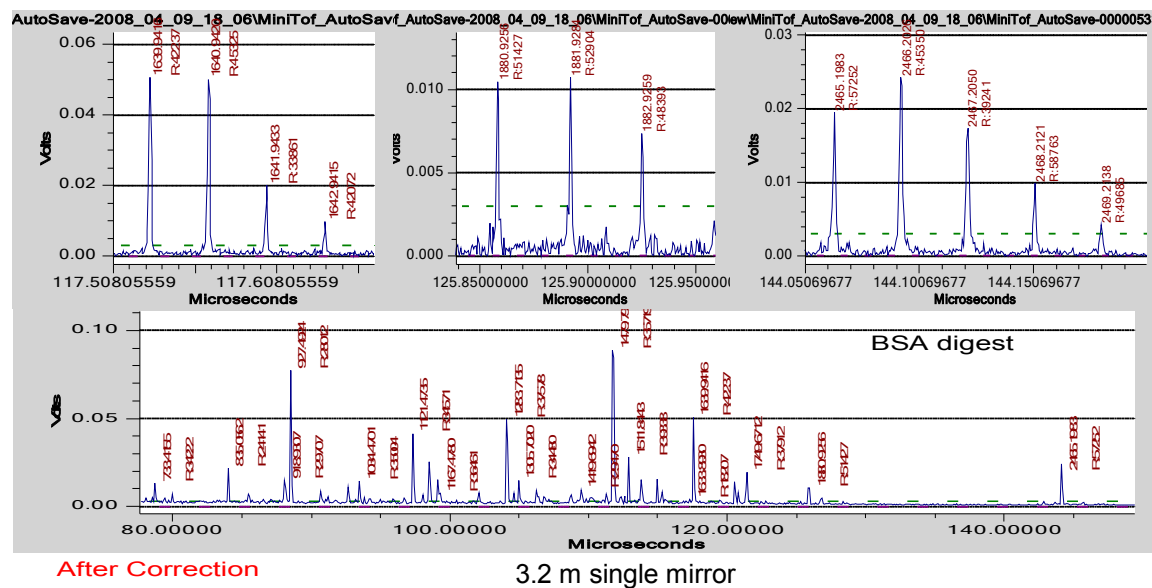
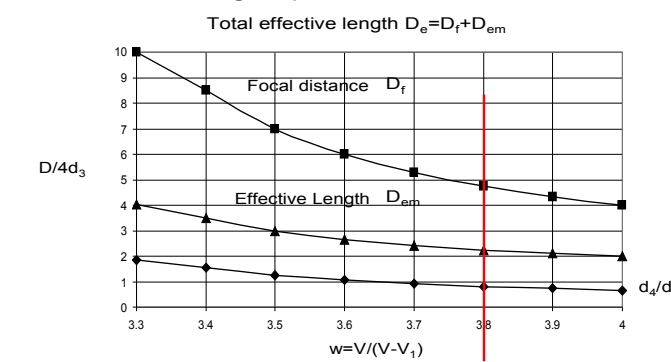
## Space and Velocity Focusing in MALDI-TOF Ion Source



**Contributions to Peak Width (dm/m):**  
 $R_{s1} = 2K^{-1}(\delta x/D_s)$      $R_{v1} = [4d_1 y/D_{em}] (\delta v_0/v_n)$   
 $R_m = R_{v1} [1 - (m/m^*)^{1/2}]$  where  $m^*$  = focused mass  
 $R_{v2} = 2K^2(\delta v_0/v_n)^2$      $R_t = 2\delta t/t = 2\delta t v_n/D_e$   
 $R_{v3} = 2K^3(\delta v_0/v_n)^3$      $\delta t$  is width of single ion pulse

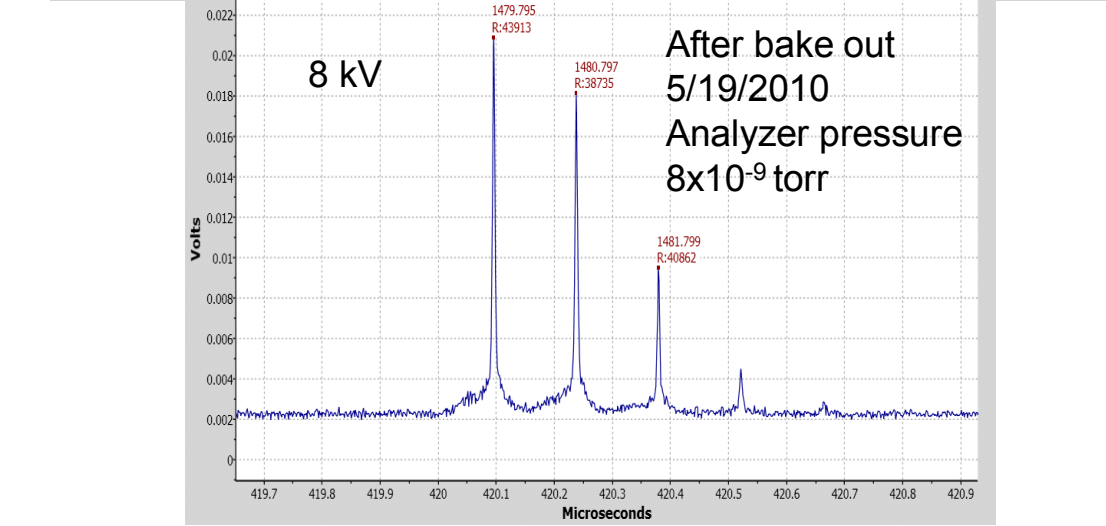
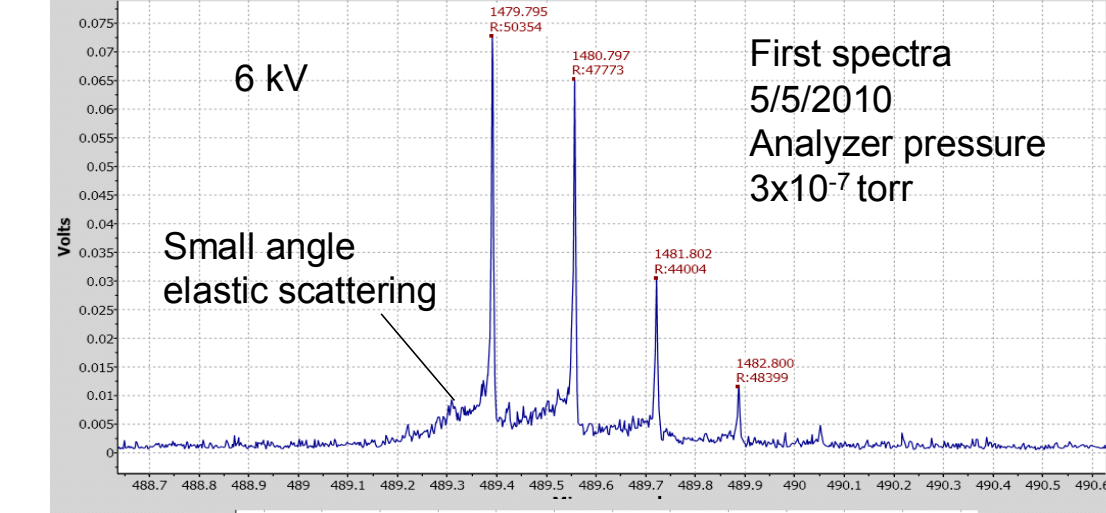
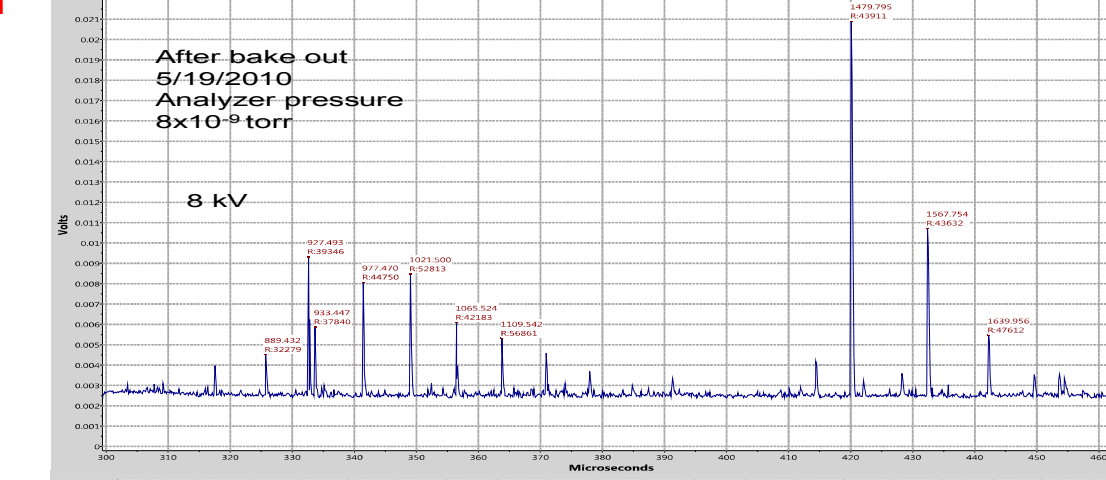
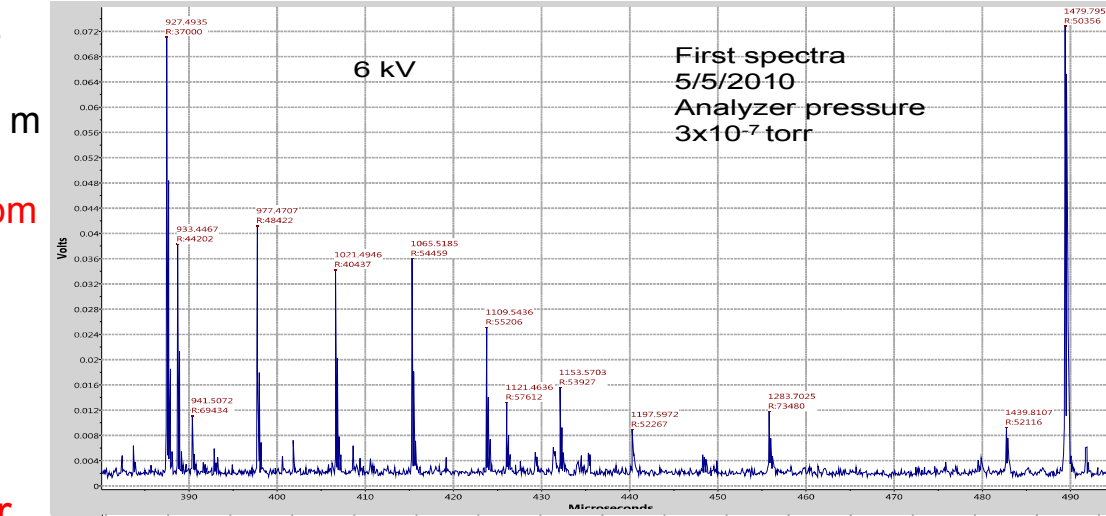
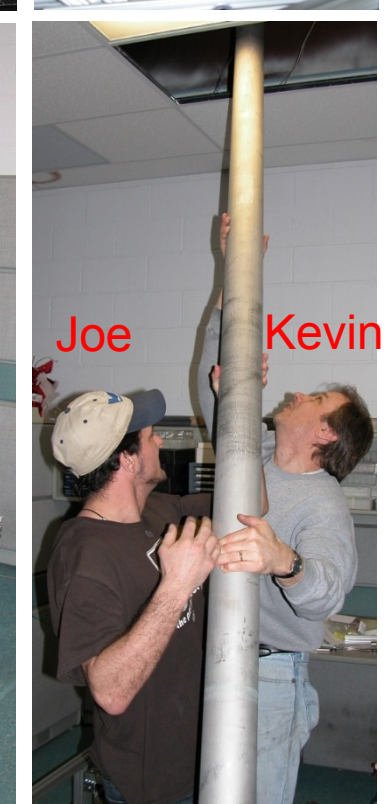
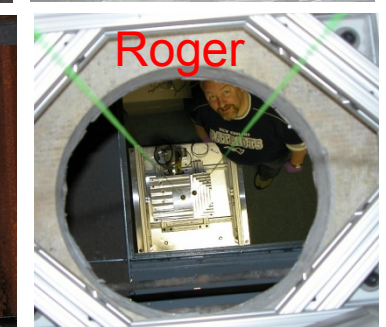


Voltage ratio  $w = V/(V-V_1)$  and  $d_4 = d_4^0(V-V_1)/(V_2-V_1)$   
 At first and second order focus  $w = 3/[1 - (4d_3/D_s)]$ ,  $V_1/V = (w-1)$  and  $V_2/V = V_1/V + (1-V_1/V)(d_4^0/d_4)$   
 $d_4^0/d_4 = (D_s/4d_3)w^{-3/2} + (w+w^{1/2})^{-1} = [w^{1/2}(w-3)]^{-1} + (w+w^{1/2})^{-1}$   
 Effective length of the mirror  $D_{em}/4d_4 = (w-3)^{-1} + 1$   
 Total effective length of the analyzer  $D_e = D_{em} + D_s + D_{t1}$  where  $D_{em} = 2d_4 y^{1/2} [1 + (d_4^0/d_4)(y^{1/2} + 1)]$   
 The principal benefit of the mirror is to increase  $D_e$  without increasing ion peak width.

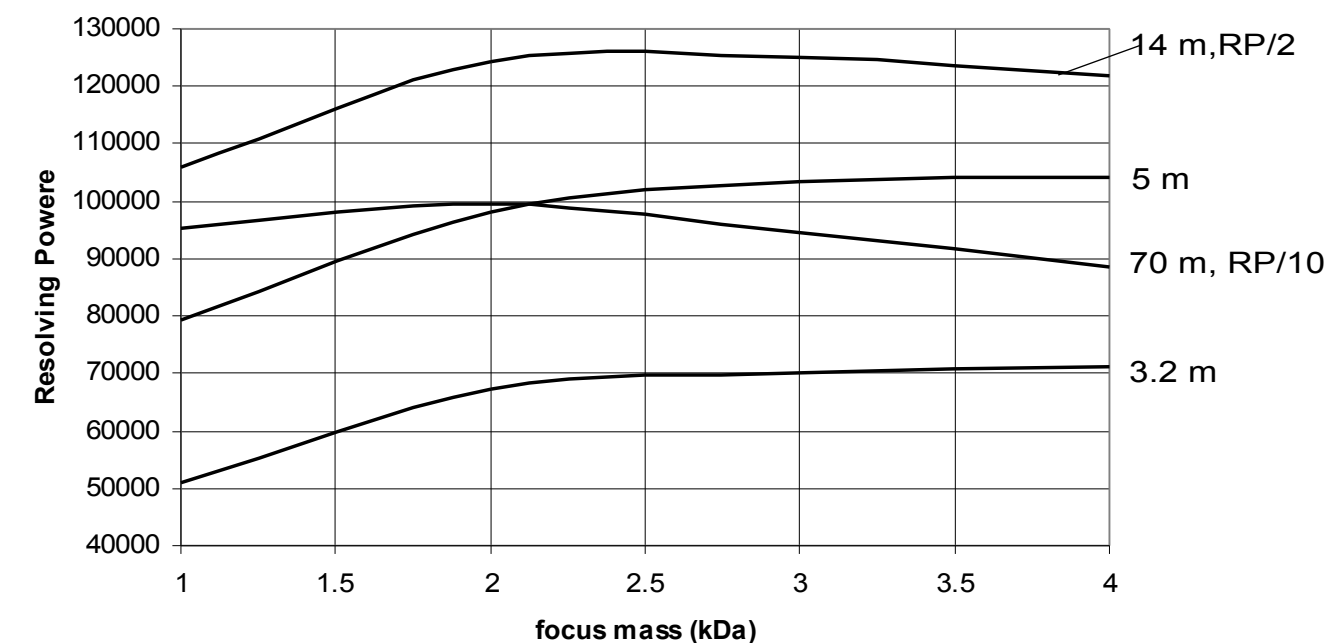


First floor

Two story MALDI MS  
 Physical Length 6m  
 Effective length 14.8 m  
 Goal is >200,000 RP  
 RMS mass error <1ppm



## Poster Number TP673



Calculated maximum resolving power at focus mass

## Present Status

Performance of 3.2 m single mirror system in good agreement with theory.

Resolving power of 5 m dual mirror system ca. 75% of theory.

- discrepancy appears to be due to combined trajectory error of 2 mirrors with relatively large deflection angle.

Initial results with 14.8 m vertical instrument off about factor of four from theoretical.

- appears to be due either to low frequency noise on HV or mechanical vibration.

## Future work

1. Obtain theoretical performance from 14.8 m system. -If not; why not?
2. Build and test 1,000,000 resolving power instrument -basic design completed but delayed until 1. above is done. -requires analyzer pressure <10^-10 torr and HV noise <1ppm

## Acknowledgements

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